

#### **Evolution Operators and Boundary Conditions for Propagation and Reflection Methods**



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#### Outline

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- Fundamental Equations
- Non-Local Boundary Conditions
- Improving Accuracy in Fast Reflection
   Calculations

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# **Part I - Fundamental Equations**



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#### **Scalar Wave Equation**

Scalar, Monochromatic Electric Field

$$\left(\frac{\partial^2}{\partial z^2} + \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + k_0^2 n^2(\vec{r})\right) \mathbf{E}(x, y, z) = 0$$

Defining  $n_0 = n_{reference}$ ,  $X_0 = \frac{1}{k_0^2 n_0^2} \frac{\partial^2}{\partial x^2}$ ,

 $Y_{0} = \frac{1}{k_{0}^{2} n_{0}^{2}} \frac{\partial^{2}}{\partial y^{2}} \text{ and } N = \frac{n^{2}(\vec{r})}{n_{0}^{2}} - 1, \text{ we have}$  $\left(\frac{\partial^{2}}{\partial z^{2}} + k_{0}^{2} n_{0}^{2} (X_{0} + Y_{0} + N)\right) E(x, y, z) = 0$ 

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#### **Forward Solution**

• Define  $H = X_0 + Y_0 + N$ . For forwardtravelling waves (  $e^{i\omega t}$  time-dependence)

$$\left(\frac{\partial}{\partial z} + ik_0 n_0 \sqrt{1+H}\right) \mathbf{E}(x, y, z) = 0$$

• We then have with  $\delta = -ik_0 n_0$  $E(x, y, z + \Delta z) = e^{\delta \Delta z \sqrt{1+H}} E(x, y, z)$ 

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### **Modal Analysis**

Modal Decomposition

$$E(x, y, \overline{z}) = \sum_{m} a_{m} E_{m}(x, y, \overline{z}) \text{ with}$$
$$\left[\frac{\partial^{2}}{\partial x^{2}} + \frac{\partial^{2}}{\partial y^{2}} + k_{0}^{2}n^{2}(x, y, \overline{z})\right] E_{m}(x, y, \overline{z}) = \beta_{m}^{2}(x, y, \overline{z}) E_{m}(x, y, \overline{z})$$

Approximate Forward Solution

$$\mathbf{E}(x, y, z + \Delta z) = \sum_{m} e^{-i\beta_{m}(x, y, \overline{z})\Delta z} \mathbf{E}_{m}(x, y, z)$$

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### **Fresnel Approximation**

Fresnel Approximation

$$\sqrt{1+H} \approx 1 + \frac{H}{2}$$

• Slowly-Varying Envelope  $E(x, y, z) = E(x, y, z)e^{-\delta z}$ 

$$\left(\frac{\partial}{\partial z} + \frac{\delta}{2}(X_0 + Y_0 + N)\right)E(x, y, z) = 0$$

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# Wide-Angle Approximations

- **Taylor Series Expansion**  $\sqrt{1+H} \approx 1 + \frac{1}{2}H - \frac{1}{8}H^2 + \frac{1}{16}H^3 - \frac{5}{128}H^4 + O(H^5)$
- Padé [2,0] approximant:  $\sqrt{1+H} \approx 1 + \frac{H}{2} - \frac{H^2}{8}$
- Padé [1,1] approximant

$$\sqrt{1+H} \approx \frac{1+3H/4}{1+H/4}$$
$$= 1 + \frac{1}{2}H - \frac{1}{8}H^2 + \frac{1}{32}H^3 - \frac{1}{128}H^4 + O(H^5)$$

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### **Square-Root Operator Recursion**

Recursion Relation

$$\sqrt{1+H} - 1 = \left(\sqrt{1+H} - 1\right)\left(\frac{\sqrt{1+H} + 1}{\sqrt{1+H} + 1}\right)$$

$$= \frac{H}{\sqrt{1+H}+1}$$
$$= \frac{H}{2+(\sqrt{1+H}-1)}$$

• Thus if  $f(x) = \sqrt{J + H} - J$  we have f(x) = x/(2 + f(x))

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### **Continued Fraction Expansion**

Iterating the recursion relation yields

$$\sqrt{1+H} - 1 = \frac{H}{2 + \frac{H}{2 + \dots \frac{H}{2 + \frac{H}{2}}}}$$

• Note that we have employed f(x) = 0to terminate the fraction, yielding a real expression.

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#### **Padé Representations**

The Padé approximant can be factored as

$$\sqrt{1+H} \approx \prod_{r=1}^{s} \left[ \frac{1+\sin^2\left(\frac{r\pi}{2s+1}\right)H}{1+\cos^2\left(\frac{r\pi}{2s+1}\right)H} \right]$$

In a partial fraction representation

$$\sqrt{1+H} = 1 + \sum_{r=1}^{s} \left[ \frac{\frac{2}{2s+1} \sin^2\left(\frac{r\pi}{2s+1}\right)H}{1 + \cos^2\left(\frac{r\pi}{2s+1}\right)H} \right]$$

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### **Finite Difference Method**

• Applying a [1,1] Padé approximant yields the Crank-Nicholson procedure

$$E(z + \Delta z) = e^{\delta \frac{H}{2}} E(z)$$
  
=  $e^{\frac{\delta}{2}(X_0 + Y_0 + N)} E(z)$   
 $\approx \left(\frac{1 + \delta H / 4}{1 - \delta H / 4}\right) E(z) + O(\delta^3)$ 

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#### **Discrete Representation**

• On a one-dimensional transverse grid  $\{x_i\}$ 

$$E(x_i, z + \Delta z) = \frac{1 - \frac{i\Delta z}{4k_0 n_0} (k_0^2 (n^2 (x_i) - n_0^2) + D_x^2)}{1 + \frac{i\Delta z}{4k_0 n_0} (k_0^2 (n^2 (x_i) - n_0^2) + D_x^2)} E(x_i, z)$$

where

$$D_x^2 E_i = \frac{E_{i+1} - 2E_i + E_{i-1}}{\Delta z^2}$$
  
and for any operator *O*,  $\frac{1}{O}$  represents  $O^{-1}$ 

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#### Part II - Nonlocal Boundary Conditions



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#### **Objective**

 To simulate on a finite, discrete computational grid the field radiated from a local source into a homogeneous semiinfinite medium.



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#### **Electrorefraction Modulator**

#### Schematic diagram of modulator



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n+ - InP substrate

NiGeAu n-contact



#### **Standard Boundary Conditions** NORTEL

Evolution of Unguided Asymmetric Field -Standard Local Transparent Boundary



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#### Improved Boundary Conditions NORTEL

Evolution of Unguided Asymmetric Field -Hybrid Boundary



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#### **Boundary Layers**

 The approximate propagation operators introduced above are unitary. To remove the outward propagating electric field at the boundary we can introduce absorbing or impedance-matched boundary layers.

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- Set  $E_0$  and  $E_{N+1}$  to be consistent with purely outgoing waves at the boundary.
  - Local Boundary Conditions:  $E_0$ ,  $E_{N+1}$  are computed from Eat the last propagation step.
  - Nonlocal Boundary Conditions:  $E_0, E_{N+1}$  are obtained from previous values of  $\exists$ .



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#### Impedance-Matched Layer

- For a non-equidistant grid,  $\Delta X_i = (1 b_i)\Delta X$ the governing equation in a homogeneous refractive index layer near the boundary is  $\left(-2ik_0n_0\frac{\partial}{\partial z} + \frac{d^2}{dx^2} + k_0^2(n_b^2 - n_0^2)\right)E(x, y, z) = 0$
- For continuous X, Z, no spurious effects.
- Thus, if  $b_i \rightarrow ia_i$ , we have

$$E_{k_x,k_z}(x,z) \propto e^{ik_x(1+ia_i)x+ik_zz}$$

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#### **Approximate and Exact Results** NORTEL

#### **Exact and Approximate Reflection Coefficients - Angle Dependence**



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#### **Continuous Nonlocal Boundary**

• Assume that  $n^2(x_{N-1}) = n^2(x_N) = n_0^2$ . At the boundary

$$\frac{\partial^2 E}{\partial x^2} = 2ik_0n_0\frac{\partial E}{\partial z}$$

• Crank-Nicholson method -  $E_j \equiv E(x, z_j)$ 

$$\frac{\partial^2}{\partial x^2} \left( \frac{E_{j+1} + E_j}{2} \right) = 2ik_0 n_0 \frac{E_{j+1} - E_j}{\Delta z}$$

• Setting  $s \equiv T_{\{-\Delta z\}} = e^{-\Delta z} \frac{\partial}{\partial z}$ , we have with  $\nu = \sqrt{4ik_0n_0/\Delta z}$ ,

$$\frac{\partial^2 E_{j+1}}{\partial x^2} = \nu^2 \frac{1-s}{1+s} E_{j+1}$$

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#### **Continuous Nonlocal Boundary**

• Outgoing condition (right boundary)

$$\frac{\partial E_{j+1}}{\partial x} = -\nu \sqrt{\frac{1-s}{1+s}} E_{j+1}$$

With  $s^{l}E(x,z) = E(x,z-l\Delta z)$ , we have

$$\frac{\partial E(x, z_{j+1})}{\partial x} + \nu E(x, z_{j+1}) = \\\nu \left[ E(x, z_j) - \frac{1}{2} E(x, z_{j-1}) + \frac{1}{2} E(x, z_{j-2}) - \frac{3}{8} E(x, z_{j-3}) + \dots \right]$$

• The electric field is optimally evaluated at  $(x_{N_w} + x_{N_w+1})/2$ .

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#### **Gaussian Beam - Continuous N.L.**

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Continuous Nonlocal Boundary Condition Gaussian Beam, 1024 Points



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#### **Remaining Power - Continuous**

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Continuous Nonlocal Boundary Condition L<sub>2</sub> Norm, 1 and 2 Gaussian Beams



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#### **Exact Nonlocal Boundary**

• With  $E_m \equiv E(x_m, z_j + \Delta z)$  the Crank-Nicholson method yields on a discrete grid

$$(1+s)(E_{m+1}-(2-k_0^2\Delta n^2)E_m+E_{m-1})=\nu^2(1-s)E_m$$

• Applying the x-translation operator  $r \equiv T_{\{-\Delta x\}} = e^{-\Delta x} \frac{\partial}{\partial x}$  $r^2 - (2 - k_0^2 \Delta n^2)r + 1 = \nu^2 \frac{1-s}{1+s}r$ 

• If the root with |r| < 1 is denoted by  $r_-$ , the discrete transparent boundary condition is

$$E_{N+1} = r_{-} \cdot E_N$$

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#### **Remaining Power - Discrete** NORTEL

**Discrete Nonlocal Boundary Condition** L<sub>2</sub> Norm, 1 and 2 Gaussian Beams



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# Padé [1,1] Boundary Conditions

• [1,1] Padé Approximation

$$-1 + \sqrt{1+H} \approx \frac{H/2}{1+H/4}$$

- **Claerbout's Equation**  $\left[ \left( 1 + \frac{H}{4} \right) \frac{\partial}{\partial z} + \delta \frac{H}{2} \right] E(x, y, z) = 0$
- Boundary Condition Equation  $(n_b = n_0)$  $\left(1 + \frac{X_0}{4}\right) \left[\frac{1-s}{\Delta z}\right] E(z + \Delta z) = -\delta \frac{X_0}{4}(1+s)E(z + \Delta z)$

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### Padé [2,0] Boundary Conditions

• [2,2] Padé Equation

$$\left(\frac{1-s}{\Delta z}\right)E_{j+1}(x) = -\delta\left(1 + \frac{X_0}{2} - \frac{X_0^2}{8}\right)\left(\frac{1+s}{2}\right)E_{j+1}(x)$$

- Laplace transform this equation with respect to X in the exterior region.
- Requiring that no poles are present in the right-hand plane of the transform yields the desired boundary condition.

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### [2,2] Boundary Condition Results



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# Padé [N,N] Boundary Conditions

• For the [N,N] case,  $sE_i(x) = E_{i-1}(x)$ , where

 $g_{i}^{(1)}(x) = \left(\frac{1 - a_{1}'\partial_{x}^{2}}{1 - a_{1}\partial_{x}^{2}}\right) E_{i-1}(x)$  $g_{i}^{(2)}(x) = \left(\frac{1 - a_{2}'\partial_{x}^{2}}{1 - a_{2}'\partial_{x}^{2}}\right) g_{i}^{(1)}(x)$ 

$$g_i^{(2)}(x) = \left(\frac{1 - a_2 \, \mathcal{O}_x}{1 - a_2 \, \mathcal{O}_x^2}\right) g_i^{(1)}(x)$$

$$g_{i}^{(k-1)}(x) = \left(\frac{1 - a_{k-1}'\partial_{x}^{2}}{1 - a_{k-1}\partial_{x}^{2}}\right)g_{i}^{(k-2)}(x)$$
$$E_{i}(x) = \left(\frac{1 - a_{k}'\partial_{x}^{2}}{1 - a_{k}\partial_{x}^{2}}\right)g_{i}^{(k-1)}(x)$$

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# **General Boundary Conditions (2)**

- Introducing a vector  $\mathbf{g}_i(x)$  with
  - $\mathbf{g}_{i,j}(x) = g_i^{(j)}(x), \ j = 1...k-1, \ \mathbf{g}_{i,k}(x) = E_i(x)$  yields

#### $(\mathbf{E} + \mathbf{A}\partial_x^2)\mathbf{g}_i(x) = 0$ with boundary conditions

$$\dot{\mathbf{g}}_{i,+} = \mathbf{B}_{+}\mathbf{g}_{i,+}, \ \dot{\mathbf{g}}_{i,-} = \mathbf{B}_{+}\mathbf{g}_{i,-}$$

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### **General Boundary Conditions (3)**

- After Laplace transforming, this yields
  - $(\mathbf{E} + p^2 \mathbf{A}) \hat{\mathbf{g}}_i(p) = \mathbf{A}(p\mathbf{g}_{i,0} + \dot{\mathbf{g}}_{i,0})$
  - or, defining  $\mathbf{C}^2 = -\mathbf{A}^{-1}\mathbf{E}$ ,

$$(p^2 \mathbf{I} - \mathbf{C}^2) \hat{\mathbf{g}}_i(p) = p \mathbf{g}_{i,0} + \dot{\mathbf{g}}_{i,0}$$

• Problem: Construct C such that all poles of  $(p\mathbf{I} + \mathbf{C})^{-1}$  have  $\Re p_i > 0$ 

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### Part III - Improving Accuracy in Fast Reflection Calculations



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#### **Facet Reflection Coefficient**

• Matching  $E_y$  and  $\frac{\partial E_y}{\partial z}$  at the boundary gives  $\begin{array}{c|c}
\Psi_y = \Psi_o^+ e^{-ik_o n_{ol} L_l z} + \Psi_o^- e^{ik_o n_{ol} L_l z} \\
\Psi_y = \Psi_o^+ e^{-ik_o n_{ol} L_l z} + \Psi_o^- e^{ik_o n_{ol} L_l z} \\
E_{yr}^{(k+1)} = \frac{1}{2} (1 - L_B L_A) (E_{yr}^{(k)} - E_{yi}), \text{ or } \\
\left[R\right]_{TE} = \frac{E_{yr}}{E_{yi}} = \frac{n_{oA} L_A - n_{oB} L_B}{n_{oA} L_A + n_{oB} L_B}
\end{array}$ 

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#### **Reflection Coefficients**



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#### **Calculated Reflection Error**

- Since the Padé approximation for *L* has poles in the evanescent spectral region, uncontrollable errors can develop.
- One method to resolve this Generate an approximant with complex coefficients by selecting an imaginary termination condition for the continued fraction representation of  $\sqrt{1+H}$ .

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#### **Complex Padé Reflection**



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### **Rotated Padé Approximants**

A second method: Write

$$\sqrt{1+H} = e^{i\alpha/2}\sqrt{1+[(1+x)e^{-i\alpha}-1]}$$

# and perform a Padé expansion in the variable

$$y = (1+x)e^{-i\alpha} - 1$$

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#### **Rotated Padé Reflection**



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#### **Refractive Index Discretization**



$$\begin{pmatrix} \Psi_{out}^{+} \\ \Psi_{out}^{-} \\ \Psi_{out}^{-} \end{pmatrix} = G \begin{pmatrix} \Psi_{in}^{+} \\ \Psi_{in}^{-} \\ \Psi_{int}^{-} \end{pmatrix} \qquad G = \begin{pmatrix} g_{11} & g_{12} \\ g_{21} & g_{22} \end{pmatrix} = T_n P_n T_{n-1} P_{n-1} \dots T_2 P_2 T_1 P_1$$

$$\textbf{Reflected field} \qquad \textbf{Transmitted field}$$

$$\Psi_{in}^{-} = -g_{22}^{-1} g_{21} \Psi_{in}^{+} \qquad \Psi_{out}^{+} = (g_{11} - g_{12} g_{22}^{-1} g_{21}) \Psi_{in}^{+}$$

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#### **Transition, Propagation Operator**



$$T_{j} = \frac{1}{2} \begin{pmatrix} 1 + \frac{n_{o_{j}}}{n_{o_{j+1}}} L_{j+1}^{-1} L_{j} & 1 - \frac{n_{o_{j}}}{n_{o_{j+1}}} L_{j+1}^{-1} L_{j} \\ 1 - \frac{n_{o_{j}}}{n_{o_{j+1}}} L_{j+1}^{-1} L_{j} & 1 + \frac{n_{o_{j}}}{n_{o_{j+1}}} L_{j+1}^{-1} L_{j} \end{pmatrix}$$

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#### **Distributed Feedback**



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#### Conclusions

- Procedures now exist for constructing exact, nonlocal boundary conditions for wide-classes of two-dimensional parabolic partial differential equations.
- Modified Padé operators can be employed to increase the accuracy of reflection calculations at abrupt interfaces.

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